

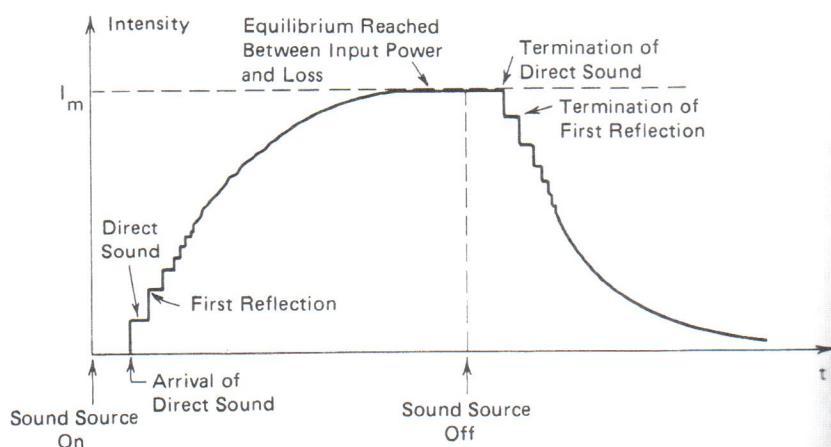


FIGURE 4.27 Typical tone intensity buildup and decay in a hall (linear scale).

of 1.5–2 s. Longer times would blur too much typical tone successions; shorter times would make the music sound “dry” and dull (see Sec. 4.8).

We may discuss a few simple mathematical relationships that appear in room acoustics. Let us imagine an enclosure of perfectly reflecting walls with no absorption whatsoever, but with a built-in *hole* of area A . Whenever the maximum intensity I_m is reached (Fig. 4.27), acoustical energy will be escaping through the hole at a rate given by the product $I_m A$.¹⁶ Since this corresponds to the steady state in which the power P supplied by the instrument equals the energy loss rate, we can set $P = I_m A$, or

$$I_m = \frac{P}{A} \quad (4.9)$$

In a real case, of course, we do not have perfectly reflecting walls with holes in them. However, we still may *imagine* a real absorbing wall as if it were made of a perfectly reflecting material with holes in it, the latter representing a fraction a of its total surface. a is called the *absorption coefficient* of the wall's material. A surface of S square meters, of absorption coefficient a , has the same absorption properties as a perfectly reflecting wall of the same size but with a hole of area $A = Sa$. Absorption coefficients depend on the frequency of the sound (usually increasing for higher frequencies), and have values that range from 0.01 (marble: an almost perfect reflector) to as much as 0.9 (acoustical tiles). Taking all this into account, we can rewrite relation (4.9) in terms of the actual wall surfaces $S_1, S_2, \dots$ with corresponding absorption coefficients $a_1, a_2, \dots$

¹⁶ It is assumed here that I_m represents the diffuse, omnidirectional sound energy flow.

$$I_m = \frac{P}{S_1 a_1 + S_2 a_2 + \dots}$$

This relation can be used to estimate wanted values of I_m , for a given instrument, and for a given distribution of absorbing wall materials.

The reverberation time τ_r is found to be a function of the hall and inversely proportional to the total absorption $A = S_1 a_1 + S_2 a_2 + \dots$. Experiments show

$$\tau_r = 0.16 \frac{V}{S_1 a_1 + S_2 a_2 + \dots}$$

with V in cubic meters, S in square meters, and a the absorption coefficients, usually increasing with increasing pitch: bass notes have longer reverberation times.

One of the problems in room acoustics is the influence (increases) the absorption properties of the walls taken into account in the design of auditoriums. If the effects related to the unpredictable sound distribution, it would be necessary to take into account the coefficient is nearly independent of wavelength. The absorbing effect of the audience is maximum at long reverberation times, such as in churches. The performer is so exposed to (and has to adapt to) the environment as an organist.

Tone distribution, buildup, and decay are dependent of the absorption coefficients and the physical characteristics of musical tones in the environment, hence on the perception of tones is deeply affected. The dependence of tones is deeply affected by the environment, and, for instance, a staccato sound is affected, depending on the reverberation properties of the environment. Finally, taking into account the dependence of tones is deeply affected by the environment. It can be shown that the resulting SPL can be shown that the resulting SPL can also fluctuate at random, introducing a recognizable timbre in a closed music space (Steinbrink, 1973).

There are other second-order effects. One of them is the phenomenon called *diffraction*. When a sound wave passes a pillar in a church or a person sitting in the audience, several phenomena may arise: (1) If the wavelength is smaller than the size (diameter) of the obstacle, the sound wave is reflected.